

A General 3-D Nonstationary GBSM for Underground Vehicular Channels

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Abstract—Reliable and efficient communications are indispensable for vehicles in underground environments. Underground wireless channels present a number of unique properties, such as guided propagation, rich scatterers, and near-field/far-field effect. In this article, a 3-D twin cluster geometry-based stochastic model (GBSM) is proposed to describe underground vehicular channel characteristics in both pillar and tunnel scenarios. The proposed model supports arbitrary trajectory mobility of vehicles and multiple antenna configurations at the transmitter (Tx) and the receiver (Rx). The cluster time evolution is modeled

by different scatterer generation and updating methods to simulate the channel characteristics such as nonstationarity, near-field/far-field differences, and waveguide effects. Based on the proposed channel model, the statistical characteristics of the channel are derived and simulated, including the temporal autocorrelation function (ACF), spatial cross-correlation function (CCF), delay power spectrum density (PSD), Doppler PSD, and so on. Besides, underground channel measurements at 2.5/3.5 GHz are conducted in a garage scenario. Comparison results of channel measurements and simulations validate the accuracy and usefulness of the proposed GBSM.

Index Terms—Communication channels, electromagnetic propagation, radio propagation, time-varying channels.

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I. INTRODUCTION

RECENTLY, the development of underground space is increasing, and the applications of underground facilities are diversifying. Due to the ground obstruction and complex underground environment, the existing mobile communication system usually cannot cover the underground space [1], [2], which requires the design and implementation of underground communication systems to ensure the full scenario coverage of next-generation wireless networks [3], [4]. Specifically, the underground vehicular communication is indispensable for underground navigation, vehicle collaboration, and realization of the intelligent transportation system (ITS). Besides, in the underground exploration and sensing, employing unmanned vehicles, including unmanned ground vehicles (UGVs), and unmanned aerial vehicles (UAVs), can be a significant solution due to their convenience and security. Reliable unmanned vehicles to unmanned vehicles and unmanned vehicles to background control center communications can ensure the accomplishment of tasks. Underground space is a kind of enclosed space, where the propagation characteristics of electromagnetic waves are different from open space. The channel model that can capture the unique characteristics of the underground vehicular channel is essential for communication system design and will play an important role in link budget, transmission scheme selection, and system performance evaluation [5], [6], [7].

For the special environment of underground space, a lot of wireless channel-related studies have been conducted based on the channel measurement, simulation, and theoretical analysis. Depending on the function of underground facilities, underground space can be divided into underground garages, tunnels, subways, mines, and so on. For the underground

garage scenario, the Aalborg University research team developed a large-scale fading channel model based on the $\alpha - \beta$ model [8], which also took into account the signal loss between multistory garages based on 800 MHz and 2 GHz channel measurements. The University of South Carolina Team proposed a nongeometric stochastic channel model based on the tap-delay-line (TDL) structure [9], which supports both line-of-sight (LoS) and nonLoS (NLoS) conditions based on channel measurement at 5 GHz. Besides, the path loss model and multipath model were established based on ultrawideband channel measurements (3.28–5.03 GHz) in the underground garage scenario at Korea Dong International University [10], [11]. Beijing Jiaotong University conducted channel measurement at 5.9 GHz in the garage scenario, and antenna array was used in the measurement to obtain the directional characteristics of the channel [12].

For the subway scenario, Lienard et al. [13] conducted channel measurements in the 900 MHz band for a metro tunnel scenario using the channel sounder. The effects of tunnel narrowing, bending, and sheltering on the channel were investigated through the analysis of parameters such as path loss and delay spread, and the feasibility of using multiple-input multiple-output (MIMO) to increase the channel capacity in tunnel scenarios was discussed [14]. Valdesueiro et al. [15] conducted channel measurements in the 5.8 GHz band, using software-defined radio equipment at both the transmitter (Tx) and the receiver (Rx) and investigated channel capacity, as well as the tradeoff between antenna spacing and diversity gain for 2×2 MIMO systems. Zhang et al. [16] combined vector parabolic equations with waveguide mode theory to model subway tunnel scenarios in the 1 and 2 GHz frequency bands. The influence of operating frequency and tunnel section shape on the signal propagation characteristics was investigated based on the parametric analysis of the received power, fading statistics, and path loss probability distribution [16]. Guan et al. [17] measured and computed propagation characteristics of a subway environment at 2.4 GHz, including near shadowing, path loss, and shadow fading.

For the tunnel scenario, Valdesueiro et al. [18] performed channel measurements at 2.6 GHz with a bandwidth of 10 MHz using a measurement platform based on the universal software radio peripheral (USRP) B210 to analyze path loss, time delay, and Doppler spread. The [19] conducted vehicle-to-vehicle (V2V) channel measurements in an arched tunnel in Madrid, using the multiple-input single-output (MISO) antenna fixed on the train. Briso-Rodruéz et al. [20] measured path loss and other large-scale fading parameters in an arched train tunnel at 900 MHz to develop a large-scale fading statistical channel model. Molina-Garcia-Pardo et al. [21] conducted channel measurements in a semicircular tunnel at 2.8–5 GHz and collected parameters such as path loss, the received signal amplitude probability density function (PDF), and the cumulative distribution function (CDF) with MIMO configuration. Qiu et al. [22] proposed an emulation TDL model for railway tunnels, considering the impact of the rolling stock.

For the mine scenario, Chehri et al. [23], [24], [25] conducted a series of measurements in the experimental mine located in Waldorf, Canada. The measurement campaign focused on ultrawideband channels at 2–5 GHz. In order to investigate the channel spatial variation, the Tx antenna was moved on a rectangular with 8×5 grids spaced 7 cm apart and

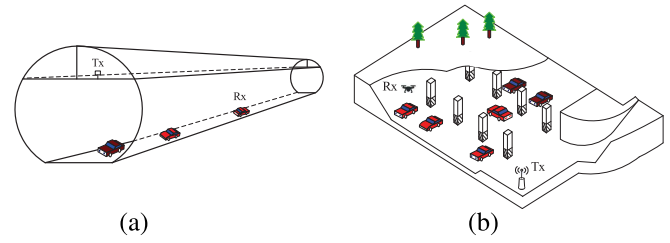


Fig. 1. Typical underground structures. (a) Tunnel structure. (b) Pillar structure.

the Rx antenna was fixed during the measurement. This reveals the large/small-scale fading and some frequency- and space-domain characteristics in the LoS and NLoS conditions. Sun and Akyildiz [26] proposed a multimode waveguide model that can characterize the fast fluctuations of the channel and give analytical expressions for the received power and channel impulse response (CIR) at arbitrary locations in the roadway. Based on this model, the authors investigated the effects of tunnel size, operating frequency, antenna position, and polarization. Linard and Degauque [27] and Ranjan et al. [28] proposed a hybrid multimode model combining waveguide and geometric-optical models to investigate the effects of surface roughness and mine wall tilt on the path loss.

Generally, the channel characteristics of underground space mainly depend on the spatial structure of the underground scenarios [29]. According to the different underground spatial structures, the underground space scenarios can be roughly divided into two types, that is, tunnel type and pillar type, as shown in Fig. 1. The tunnel structure scenarios contain subway tunnels, train tunnels, highway tunnels, mine roadways, and some other scenarios, in which the electromagnetic waves will be reflected between the walls many times to form the guided propagation. The pillar structure scenarios usually contain underground garage and pit face of mine, which have rich scatterers, for example, support pillars and parked vehicles. For clarity, significant channel properties in tunnel and pillar scenarios are listed in Table I. The existing researches on underground space channel mainly focus on exploring and analyzing the channel characteristics of different scenarios and lack a common channel model for different structure scenarios. The development of a general underground channel model supporting different underground structures and transceiver moving modes are indispensable for underground propagation mechanism simulation, which is very important to the Antennas and Propagation Community.

This article addresses the problem of nonstationary underground channel modeling. The proposed underground channel model is applicable to both tunnel and pillar scenarios and can support arbitrary trajectory mobility of vehicles, as well as multiple antenna configurations. Compared with previous works modeling underground channels [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18], [19], [20], [21], [22], [23], [24], [25], [26], [27], [28] and open space vehicular and UAV channels [30], [31], [32], [33], [34], [35], the contributions and innovations of this article are summarized as follows.

- 1) A general nonstationary geometry-based stochastic model (GBSM) is proposed for two types of underground vehicular channels (tunnel scenario and pillar scenario) by considering different channel characteristics

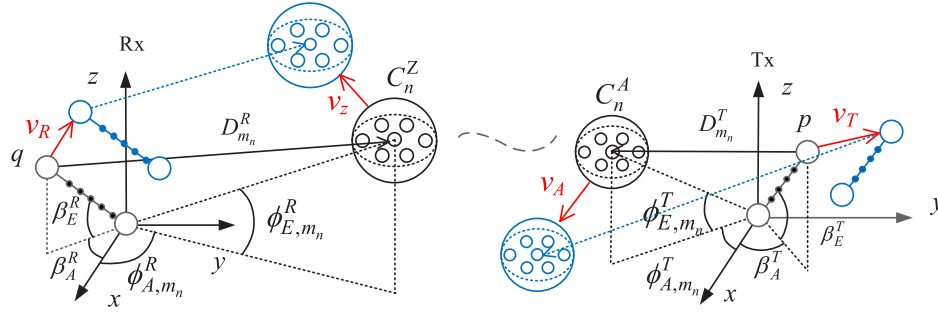


Fig. 2. 3-D wideband twin cluster channel model framework.

TABLE I
CHANNEL PROPERTIES IN UNDERGROUND SCENARIOS

	Waveguide/cluster/scatterer properties
Tunnel	Obvious waveguide effect
	Near-field/far-field channel difference
	Aperture effect lead to convergent clusters parameters
Pillar	Non-obvious waveguide effect
	MPCs mainly come from near scatterers
	The clutter distribution of scatterers in enclosed space

brought by different underground structure scenarios, including waveguide effect, near/far-field effect, and the enclosed property of underground space.

- 2) Channel statistical properties of the proposed underground channel model, including delay/angular/Doppler power spectrum density (PSD), the space-time-frequency correlation function (STF-CF), level-cross rate (LCR), average fading duration (AFD), and stationary interval, are thoroughly derived and simulated. Vehicular MIMO channel characteristics in different underground scenarios are compared through simulation results.
- 3) Underground channel measurements are conducted at 2.5/3.5 GHz and some simulation parameters are obtained by fitting measurement data. The measurement results are compared with simulation results, validating the accuracy and usefulness of the proposed channel model.

The rest of this article is organized as follows. In Section II, the geometry construction and parameter generation methods of the proposed channel model are described. In Section III, derivations of statistical properties such as delay PSD, STF-CF, LCR, and AFD are provided. In Section IV, channel simulation results in different underground scenarios are analyzed. Channel model validation through channel measurement is provided in Section V. Conclusions are drawn in Section VI.

II. 3-D WIDEBAND UNDERGROUND MIMO GBSM

The underground space usually has abundant scatterers and enclosed space. Multibounce multipath components (MPCs) account for a considerable proportion in the whole CIR. In this case, the application of the general geometric stochastic

modeling method or ray-tracing method to generate the MPCs will lead to unnecessary computation [36]. To address this problem, the twin cluster modeling framework abstracting the propagation between the first and last bounce as a virtual link can reduce the computation and improve the simulation efficiency greatly [37], [41]. Furthermore, to characterize different channel properties in tunnel or pillar scenarios, based on the twin cluster model framework, we fine two different ways to generate and update the cluster level parameters. Channel properties are reflected in generation of the simulation parameters, which ensures the generality of the proposed model.

The twin cluster model is shown schematically in Fig. 2, and the key parameters involved in the proposed model are listed in Table II. Considering that electromagnetic wave propagation in underground scenarios will experience large- and small-scale fading, the MIMO wideband fading channels can be represented by CIR matrix

$$\mathbf{H} = [PL \cdot SH]^{1/2} \cdot \mathbf{H}_s \quad (1)$$

where PL is the path loss caused by propagation distance between the Tx and Rx. Shadowing is represented by SH . Matrix $\mathbf{H}_s$ represents small-scale fading. Due to different path loss exponent at near-field and far-field in underground scenario, we use two-slope large-scale fading model, that is,

$$PL = \begin{cases} A_1 + n_1 10 \log_{10}(d), & \text{if } d \leq r_{bp} \\ B_1 + n_2 10 \log_{10}(d), & \text{if } d > r_{bp} \end{cases} \quad (2)$$

where d is the distance between Tx and Rx, r_{bp} is the break point dividing the near-field and far-field, and usually takes the value of $r_{bp} = \max\{w^2/\lambda, h^2/\lambda\}$, where w and h are cross-sectional dimensions. Parameters A_1 , A_2 , n_1 , and n_2 can be obtained by channel measurement or simulation. Note that the break point not only separates near/far fields with different large-scale fading properties in waveguide transmission, but also separates near/far fields with different small-scale fading properties [29].

Small-scale channel fading is resulted from multipath propagation caused by objects and walls in underground space. A typical 3-D MIMO channel between Tx having n_T antenna elements and Rx having n_R antenna elements is illustrated in Fig. 2. Scatterers in the real world are abstracted as a number of scattering clusters. For the sake of simplicity, only the n th cluster is presented in figure. Meanwhile, the first and last bounce clusters are represented by sphere beside Tx, C_n^A , and sphere beside Rx, C_n^Z , respectively. The propagation path between C_n^A and C_n^Z can be denoted as a virtual link having a randomly generated delay. Besides, when a path propagates

through single bounce, the delay of the virtual link will be zero. This channel modeling framework supports mobility of Tx, Rx, C_n^A , and C_n^Z , that is, time-variant coordinates $\vec{A}_0^T$, $\vec{A}_0^R$, $\vec{C}_n^A$, and $\vec{C}_n^Z$. Let ϕ_{A,m_n}^T and ϕ_{E,m_n}^T denote the azimuth and elevation angles of departure (AAoD/EAoD) of the m th ray in cluster C_n^A , respectively. Let ϕ_{A,m_n}^R and ϕ_{E,m_n}^R denote azimuth and elevation angles of arrival (AAoA/EAoA) of the m th ray in cluster C_n^Z . Similarly, let $\phi_{A,LoS}^T$, $\phi_{E,LoS}^T$, $\phi_{A,LoS}^R$, and $\phi_{E,LoS}^R$ stand for the AAoD, EAoD, AAoA, and EAoA of the LoS path, respectively.

The small-scale fading of the wideband MIMO channel can be described as a matrix $\mathbf{H}_s = [h_{pq}(t, \tau)]_{n_T \times n_R}$. The entries of $\mathbf{H}_s$ consist of two components, that is, the LoS and NLoS components, and is written as

$$h_{pq}(t, \tau) = \sqrt{\frac{K_R}{K_R + 1}} h_{pq}^{\text{LoS}}(t, \tau) + \sqrt{\frac{1}{K_R + 1}} h_{pq}^{\text{NLoS}}(t, \tau) \quad (3)$$

where K_R is the Ricean K -factor. The NLoS components $h_{pq}^{\text{NLoS}}(t, \tau)$ is written as

$$\begin{aligned} h_{pq}^{\text{NLoS}}(t, \tau) &= \sum_{n=1}^{N(t)} \sum_{m=1}^{M_n} \left[\begin{array}{c} F_{q,V}(\phi_{E,m_n}^R, \phi_{A,m_n}^R) \\ F_{q,H}(\phi_{E,m_n}^R, \phi_{A,m_n}^R) \end{array} \right]^T \\ &\times \left[\begin{array}{cc} e^{j\theta_{mn}^{VV}} & \sqrt{\kappa_{mn}^{-1}} e^{j\theta_{mn}^{VH}} \\ \sqrt{\kappa_{mn}^{-1}} e^{j\theta_{mn}^{HV}} & e^{j\theta_{mn}^{HH}} \end{array} \right] \left[\begin{array}{c} F_{p,V}(\phi_{E,m_n}^T, \phi_{A,m_n}^T) \\ F_{p,H}(\phi_{E,m_n}^T, \phi_{A,m_n}^T) \end{array} \right] \\ &\cdot \sqrt{P_{pq,m_n}(t)} \cdot e^{j2\pi f_c \tau_{pq,m_n}(t)} \cdot \delta(\tau - \tau_{pq,m_n}(t)) \end{aligned} \quad (4)$$

where $\{\cdot\}^T$ represents transposition, and f_c denotes the carrier central frequency. Functions $F_{p,V/H}$ and $F_{q,V/H}$ are the antenna patterns of Tx and Rx, the superscripts V and H denote vertical polarization and horizontal polarization, respectively. Besides, κ_{mn} denotes the cross polarization power ratio, θ_{mn}^{VV} , θ_{mn}^{VH} , θ_{mn}^{HV} , and θ_{mn}^{HH} denote the random phases uniformly distributed within $(0, 2\pi]$, $P_{pq,m_n}(t)$ and $\tau_{pq,m_n}(t)$ are the normalized power and delay of the m th ray in the n th cluster at time t , respectively. For the LoS component, it can be written as

$$\begin{aligned} h_{pq}^{\text{LoS}}(t, \tau) &= \left[\begin{array}{c} F_{q,V}(\phi_{E,LoS}^R, \phi_{A,LoS}^R) \\ F_{q,H}(\phi_{E,LoS}^R, \phi_{A,LoS}^R) \end{array} \right]^T \left[\begin{array}{cc} e^{j\theta_{LoS}^{VV}} & 0 \\ 0 & e^{j\theta_{LoS}^{HH}} \end{array} \right] \\ &\times \left[\begin{array}{c} F_{p,V}(\phi_{E,LoS}^T, \phi_{A,LoS}^T) \\ F_{p,H}(\phi_{E,LoS}^T, \phi_{A,LoS}^T) \end{array} \right] \\ &\cdot e^{j2\pi f_c \tau_{pq,LoS}(t)} \delta(\tau - \tau_{pq,LoS}(t)) \end{aligned} \quad (5)$$

where θ_{LoS}^{VV} and θ_{LoS}^{HH} are random phases that uniformly distributed within $(0, 2\pi]$, and $\tau_{pq,LoS}$ refer to the delay of LoS component.

In the proposed model, channel simulation parameters can be divided into two categories: 1) large-scale parameters (LSPs) including delay spread, Ricean K -factor, shadowing fading, and AAoA/EAoA/AAoD/EAoD spreads generated in simulation initialization step and 2) small scale parameters (SSPs) including AAoAs, EAoAs, AAoDs, EAoDs, time delays, phases, and powers for different clusters, which will be generated or updated at each time instants [47].

The channel simulation process has two stages, that is, model initialization and time evolution. In the model initialization stage, the scenario types, antenna parameters, Tx/Rx trajectories, and LSPs are generated first. Then the

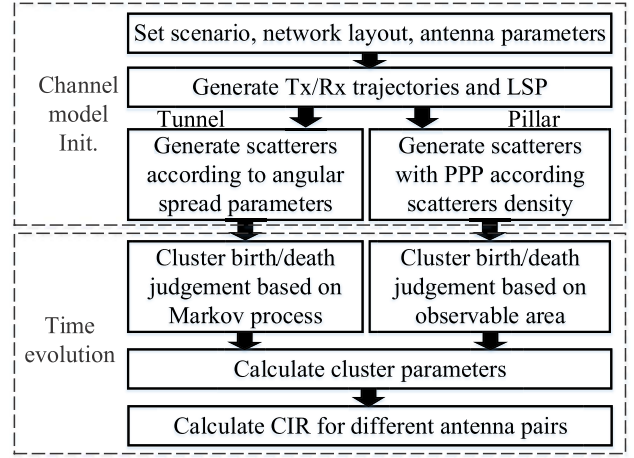


Fig. 3. Flowchart of the channel simulation process.

initial scattering cluster parameters are generated according to the scenario structure type. For channel simulation process in tunnel and pillar scenarios, the detailed flowchart is presented in Fig. 3.

For the tunnel structure scenario, since the centrality of clusters in angular domain, the angle spread, cluster generation, and recombination rates are used to generate the scattering clusters concentrated in the tunnel trending direction. For the pillar scenario, since the randomness of scatterer distribution, the Poisson point process (PPP) is used to generate randomly distributed scattering clusters in the finite space.

Due to the motions of the Tx, Rx, and scatterers, the channel will present nonstationarity, that is, channel parameters vary with time. It means that channel parameters should be updated at each time instant during simulation. Based on the channel sampling theorem in [43], the time-variant channel can be divided into a series of segments by time interval Δt_{BD} , and in each time interval the channel can be seen as constant. The maximum time interval can be determined according to Doppler bandwidth as

$$\Delta t_{BD} \leq \frac{1}{2B_D} = \frac{\lambda}{4 \max |\vec{v}_T - \vec{v}_R + \vec{v}_Z - \vec{v}_A|} \quad (6)$$

where B_D is the width of the Doppler spectrum, and $\vec{v}_T$, $\vec{v}_R$, $\vec{v}_A$, and $\vec{v}_Z$ represent the vector of velocities at Tx, Rx, C_n^A , and C_n^Z . Since the open property of the tunnel scenario, MPCs from distant scatterers have considerable effect on channels, while in the pillar scenario, MPCs from distant scatterers will be obstructed by near scatterers. For each time interval, depending on scenario types, we implement the cluster birth/death algorithm based on the Markov process and the observable region and update the parameters of the surviving clusters to finally generate the corresponding CIR.

A. Cluster Generation and Time Evolution in Tunnel Scenario

Considering the channel characteristics of the tunnel scenario and the demand of mobile communication between flexible moving vehicles, we use the channel parameter generation method and time evolution mechanism adapted to the corresponding channel characteristics. Specifically, we set different delay spread σ_τ , angle spreads $AS(\phi_{A,m_n}^T/\phi_{E,m_n}^T/\phi_{A,m_n}^R/\phi_{E,m_n}^R)$,

TABLE II
DEFINITIONS OF MAIN PARAMETERS OF THE PROPOSED CHANNEL MODEL

Symbol	Definition
$\vec{A}_0^T / \vec{A}_0^R$	Position vectors of first transmit/receive antenna elements
$\vec{C}_n^A / \vec{C}_n^Z$	Position vectors of clusters C_n^A / C_n^Z
$\vec{C}_{m_n}^A / \vec{C}_{m_n}^Z$	Position vectors of m -th ray in clusters C_n^A / C_n^Z
β_A^T / β_A^R	Azimuth angles of the transmit/receive antenna array broadside
β_E^T / β_E^R	Elevation angles of the transmit/receive antenna array broadside
δ_T / δ_R	Antenna spacings of the transmit/receive arrays
$\phi_{A,m_n}^T / \phi_{E,m_n}^T$	Azimuth and elevation angles between C_n^A and transmit antenna element via m -th ray
$\phi_{A,m_n}^R / \phi_{E,m_n}^R$	Azimuth and elevation angles between C_n^Z and receive antenna element via m -th ray
$\phi_{A,LoS}^T / \phi_{E,LoS}^T$	AAoD and EAoD of the LoS component
$\phi_{A,LoS}^R / \phi_{E,LoS}^R$	AAoA and EAoA of the LoS component
D_n^T / D_n^R	Distances from transmit/receive to C_n^A / C_n^Z
$D_{m_n}^R / D_{m_n}^T$	Distances between transmit/receive antenna element and C_n^A / C_n^Z via m -th ray

and cluster birth/death control parameters $\lambda_G(\lambda_R)$ for near-field and far-field according to whether the Tx–Rx distance is larger than break point distance r_{bp} . The temporal nonstationarity of the channel can be caused by the motion of the transceiver, and we introduce variable $\delta_P(t, \Delta t_{BD})$ to describe the variation in the transmission environment from time t to $t + \Delta t_{BD}$. It represents the sum of the distances traveled by the Tx and Rx from time t to $t + \Delta t_{BD}$, that is,

$$\delta_P(t, \Delta t_{BD}) = v_T(t) \Delta t_{BD} + v_R(t) \Delta t_{BD}. \quad (7)$$

Then, the probability of a cluster survived in this period can be represented by

$$P_s(t, \Delta t_{BD}) = \exp \left[-\lambda_R \left(\frac{\delta_P(t, \Delta t_{BD})}{D_c} \right) \right] \quad (8)$$

where D_c is a scenario-dependent coefficient controlling the spatial correlation. Typical values of D_c can be chosen with the same order of correlation distance [37].

We consider all clusters having the same probability of survival. According to the definition of the Markov birth-death process, the clusters of a channel at moment $t + \Delta t_{BD}$ are considered to be the sum of the clusters that survive from moment t and the clusters that are generated at time intervals Δt_{BD} . The birth and dead process is determined by cluster generation and recombination rates (λ_G/λ_R). Consequently, the mean value of the cluster number in the channel has the expression as

$$\mathbb{E}[N(t)] = \frac{\lambda_G}{\lambda_R}. \quad (9)$$

Based on the Markov birth death concept, the time interval between the creation and disappearance of the clusters follows an exponential distribution. The mean value of the number of new clusters can be expressed as

$$\mathbb{E}[N_{\text{new}}(t + \Delta t_{BD})] = \frac{\lambda_G}{\lambda_R} (1 - P_s(t, \Delta t_{BD})). \quad (10)$$

For each newly generated cluster, the 3-D coordinate of the cluster center are generated through the Tx/Rx near-field/far-field channel parameters, and due to the aperture effect in

the tunnel scenario, the scattered clusters will usually be concentrated in the direction of the tunnel, and different angular spread can be used to characterize the spread of the scattered clusters in different regions. For the azimuth and elevation angles from the Rx to the center of the last bounce cluster, the angles can be expressed as

$$\phi_{A,n}^R = \text{AS}(\phi_{A,n}^R) Y_{A,n}^R + \psi_{A,n}^R \quad (11)$$

$$\phi_{E,n}^R = \text{AS}(\phi_{E,n}^R) Y_{E,n}^R + \psi_{E,n}^R \quad (12)$$

where $\text{AS}(\phi_{A,n}^R)$ and $\text{AS}(\phi_{E,n}^R)$ denote the azimuth and elevation angular spreads of the arrival angle, respectively, $Y_{A,n}^R$ and $Y_{E,n}^R$ follow the normal distribution $N(0, 1)$, and $\psi_{A,n}^R$ and $\psi_{E,n}^R$ denote the average of the azimuth and elevation angles, respectively. To determine the coordinate of the center of the last bounce scattering cluster with respect to (w.r.t.) to the Rx, a distance parameter is required according to scale of tunnel

$$D_n^R = \begin{cases} \frac{z - A_{0,z}^R}{\sin \phi_{E,n}^R} \tan \phi_{A,n}^R (z - A_{0,z}^R) + A_{0,y}^R \in (y_{lw}, y_{rw}) & \text{if } \frac{\tan \phi_{E,n}^R}{y - A_{0,y}^R} \\ \frac{\cos \phi_{A,n}^R \sin \phi_{E,n}^R}{\tan \phi_{A,n}^R (z - A_{0,z}^R) + A_{0,y}^R \notin (y_{lw}, y_{rw})} & \text{if } \frac{\tan \phi_{E,n}^R}{y - A_{0,y}^R} \end{cases} \quad (13)$$

where $A_{0,x}^R$, $A_{0,y}^R$, and $A_{0,z}^R$ are x , y , and z components of the Rx coordinate, y denotes the side wall of the tunnel, depending on $y = y_{lw}$ for the left side wall and $y = y_{rw}$ for the right side wall, and z denotes the ceiling and bottom of the tunnel, depending on $z = z_t$ for ceiling and $z = z_b$ for bottom.

Similarly, the coordinates of the center of the first bounce scattering cluster with respect to the Tx can be obtained in the same way using the departure parameters azimuth and elevation angle spreads $\text{AS}(\phi_{A,n}^R/\phi_{A,n}^R)$ and the distance parameter D_n^T . Subsequently, the 3-D coordinates of the

scattering cluster and the center can be expressed as

$$\vec{C}_n^A = \vec{A}_0^T + \vec{D}_n^T \quad (14)$$

$$\vec{C}_n^Z = \vec{A}_0^R + \vec{D}_n^R \quad (15)$$

where $\vec{D}_n^T$ and $\vec{D}_n^R$ denote vectors from Tx/Rx to the scatterer center, that is,

$$\vec{D}_n^T = D_n^T \cdot [\cos \phi_{A,n}^T \cos \phi_{E,n}^T \sin \phi_{A,n}^T \cos \phi_{E,n}^T \sin \phi_{E,n}^T]^T$$

$$\vec{D}_n^R = D_n^R \cdot [\cos \phi_{A,n}^R \cos \phi_{E,n}^R \sin \phi_{A,n}^R \cos \phi_{E,n}^R \sin \phi_{E,n}^R]^T.$$

Finally, due to the spread of a scattering cluster in space, we use a 3-D Gaussian distribution to describe the dispersion of different scattering points in a scattering cluster, and for the m th subpath in the twin cluster C_n^A and C_n^Z , the coordinates of the scattering points can be expressed as

$$\vec{C}_{m_n}^{A/Z} = \vec{C}_n^{A/Z} + [\Delta x_{m_n}^{A/Z} \Delta y_{m_n}^{A/Z} \Delta z_{m_n}^{A/Z}]^T \quad (16)$$

where $[\Delta x_{m_n}^{A/Z} \Delta y_{m_n}^{A/Z} \Delta z_{m_n}^{A/Z}]^T$ follows the 3-D Gaussian distribution with variance σ_n^2 .

B. Cluster Generation and Time Evolution in the Pillar Scenario

Considering that the scatterers in the pillar scenario are distributed in the finite space and usually are concentrated near the transceiver, we use a different approach to generate scattering clusters from the tunnel scenario. First, we use the PPP in finite space to generate the expected number of cluster centers in the underground space. The coordinates set of the cluster centers can be expressed by matrix $\mathbf{C}_{\text{tot}} = [\vec{C}_1 \ \vec{C}_2 \ \dots \ \vec{C}_{N_{\text{tot}}}]^T$, where $N_{\text{tot}} = \text{Poisson}(\lambda_s L)$, and λ_s and L denote the scatterer density and volume of underground space. To generate the Poisson-distributed scatterer number, we use the stop time method [48]

$$N_{\text{tot}} = \max \left\{ k \mid \sum_{i=1}^k \log(U_i) < -\lambda_s L \right\} \quad (17)$$

where U_i follows uniform distribution in (0,1). Due to the spread of each cluster in the pillar scenario, then we use (15) to generate the scattering points in each scattering cluster.

Algorithm 1 Time Evolution in a Pillar Scenario

Input: $\vec{A}_0^T, \vec{A}_0^R, \mathbf{C}_{\text{tot}}, d_{\text{lim}}, N_{\text{tot}}$

Output: $\mathbf{C}_{\text{tot}}^A, \mathbf{C}_{\text{tot}}^Z$

```

1 Initialize  $i = 0, j = 0;$ 
2 for  $n \in [1, N_{\text{tot}}]$  do
3    $d_n^T = \text{norm}(\vec{C}_n - \vec{A}_0^T)$   $d_n^R = \text{norm}(\vec{C}_n - \vec{A}_0^R)$  if
    $d_n^T < d_{\text{lim}}$  then
4      $\vec{C}_i^A = \vec{C}_n; i = i + 1$ 
5   end
6   if  $d_n^R < d_{\text{lim}}$  then
7      $\vec{C}_j^Z = \vec{C}_n; j = j + 1$ 
8   end
9 end
10  $\mathbf{C}_{\text{tot}}^A = \text{repmat}([\vec{C}_1^A \ \vec{C}_2^A \ \dots \ \vec{C}_i^A], 1, j)$ 
11  $\mathbf{C}_{\text{tot}}^Z = \text{repelem}([\vec{C}_1^Z \ \vec{C}_2^Z \ \dots \ \vec{C}_j^Z], 1, i)$ 

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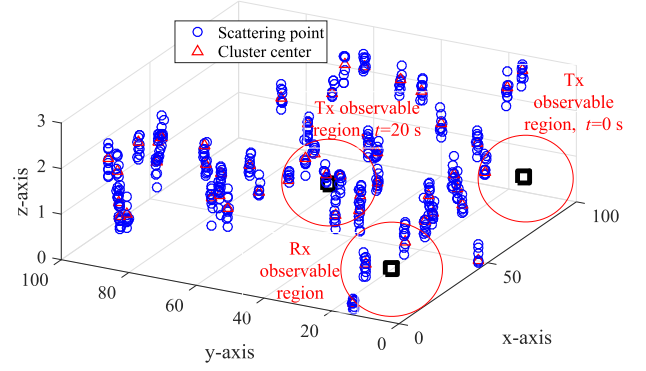


Fig. 4. Cluster generation using PPP in a pillar scenario ($|\vec{v}_T| = 3$ m/s, $|\vec{v}_R| = |\vec{v}_Z| = |\vec{v}_A| = 0$ m/s).

As for the time evolution in the pillar scenario, since scatterers in the far region will be sheltered by scatterers in the near region, only scatterers beside Tx and Rx should be considered in channel simulations. We set the scattering clusters observable regions at Tx and Rx, respectively. At each time interval, we first determine whether the cluster in the previous time interval is still in the Tx/Rx observable regions, remove the clusters that are not in the visible regions, and add the clusters that are newly generated in the visible regions to complete the birth/death evolution process. We assume that each scatterer in the Tx observable and in Rx observable regions can form a path. At each time instant t , the cluster sets of first bounce and last bounce can be obtained by Algorithm 1. It is worth mentioning that column vectors in $\mathbf{C}_{\text{tot}}^A$ and $\mathbf{C}_{\text{tot}}^Z$ represent the coordinates of first bounce and last bounce scatterers, that is, $\vec{C}_n^A = \mathbf{C}_{\text{tot}}^A(:, n)$ and $\vec{C}_n^Z = \mathbf{C}_{\text{tot}}^Z(:, n)$.

Fig. 4 illustrates the generation of scatterers in the pillar scenario. Red circles represent the observable region at the Tx side and Rx side. Note that with movement of Tx, the observable region of Tx is changing, causing the cluster birth/death phenomenon. Besides, for clarity, scenario-specific channel simulation parameters are listed in Table III. For the tunnel scenario, the angular spread parameters are set referring to the arched tunnel measurement results in [38] and cluster generation/recombination rates are chosen according to the conclusions mentioned in [39], that is, the higher-order MPCs have a faster decay rate in the far-field, resulting in the less cluster number in the far-field region. In terms of the pillar scenario, the scenario size is chosen as a medium size underground parking lot, and the scatterer intensity and radius of the cluster visible region are set according to [40]. Note that the radius of the cluster visible region is a parameter ranging from tens of meters to hundreds of meters and can be defined by users according to the propagation environment. Without the loss of generality, the value of visible region radius is set to 20 m in the simulation.

C. Channel Parameter Calculation

After completing the generation of the scattering cluster parameters and the evolution of the birth/death process in each time interval, we use the Tx, Rx, and scatterers geometry relationship and the parameter generation method to generate corresponding cluster delay, power, and phase. For the antenna pair between the p th transmit antenna element and the q th

TABLE III
SCENARIO-SPECIFIC PARAMETERS

Tunnel	λ_G	λ_R	AS(ϕ_A^T/ϕ_A^R)	AS(ϕ_E^T/ϕ_E^R)
Near-field	20	1	0.41	0.18
Far-field	5	1	0.13	0.05
Pillar	λ_s	d_{lim}	Size of pillar scenario	
/	0.005	20 m	100 m×100 m×3 m	

receive antenna element, the departure and arrival vectors of the m th ray in the n th cluster are expressed by

$$\vec{r}_{p,m_n}^T = \vec{C}_{m_n}^A - \vec{A}_p^T \quad (18)$$

$$\vec{r}_{q,m_n}^R = \vec{C}_{m_n}^Z - \vec{A}_q^R \quad (19)$$

where $\vec{A}_p^T$ and $\vec{A}_q^R$ denote the 3-D position vectors of the p th transmit antenna element and the q th receive antenna element, and can be written as

$$\vec{A}_p^T = \vec{A}_0^T + (p-1)\delta_T \begin{bmatrix} \cos \beta_A^T \cdot \cos \beta_E^T \\ \sin \beta_A^T \cdot \cos \beta_E^T \\ \sin \beta_E^T \end{bmatrix} \quad (20)$$

$$\vec{A}_q^R = \vec{A}_0^R + (q-1)\delta_R \begin{bmatrix} \cos \beta_A^R \cdot \cos \beta_E^R \\ \sin \beta_A^R \cdot \cos \beta_E^R \\ \sin \beta_E^R \end{bmatrix}. \quad (21)$$

Then the AAoA, AAoD, EAoA, and EAoD of the m th ray in the n th path can be obtained by

$$\phi_{A,m_n}^{T/R} = \arctan_2(r_{m_n,y}^{T/R}, r_{m_n,x}^{T/R}) \quad (22)$$

$$\phi_{E,m_n}^{T/R} = \arcsin(r_{m_n,z}^{T/R}, D_{m_n}^{T/R}) \quad (23)$$

where $r_{m_n,x}^{T/R}$, $r_{m_n,y}^{T/R}$, and $r_{m_n,z}^{T/R}$ stand for x , y , and z coordinates of $\vec{r}_{m_n}^{T/R}$, and $D_{m_n}^{T/R}$ denotes the norm of $\vec{r}_{m_n}^{T/R}$. For clarity, the antenna element index subscripts (p/q) are dropped.

Simultaneously, the AAoA, AAoD, EAoA, EAoD, and length of the LoS component can be calculated from the vector of the LoS component, which can be written as

$$\vec{r}_{pq}^{\text{LoS}} = \vec{A}_p^T - \vec{A}_q^T. \quad (24)$$

Similar to (22), (23), the AAoA, AAoD, EAoA, and EAoD of the LoS component can be calculated through inverse trigonometric function, and the propagation distance of the LoS component, D_{pq}^{LoS} , can be calculated as the norm of $\vec{r}_{pq}^{\text{LoS}}$. The delay and power of MPCs are determined by the propagation distance. For the m th ray in the n th path, the propagation delay can be expressed as

$$\tau_{pq,m_n}(t) = (D_{p,m_n}^T + D_{q,m_n}^R)/c + \tilde{\tau}_n \quad (25)$$

where $\tilde{\tau}_n$ is the time delay of virtual link between first and last bounces clusters, that is, C_n^A and C_n^Z , and can be represented by $\tilde{\tau}_n = \tilde{d}_n/c + \tau_{\text{C,link}}$, in which $\tilde{d}_n$ denotes the distance between C_n^A and C_n^Z , and $\tau_{\text{C,link}}$ is an exponentially distributed variable that can be generated by

$$\tau_{\text{C,link}} = -r_\tau \sigma_\tau \cdot \ln u_n \quad (26)$$

where u_n is generated according to uniform distribution in (0, 1), r_τ denotes the delay scalar, and σ_τ denotes the delay

spread [41]. Subsequently, the power of the m th ray in the n th path is determined by

$$P'_{pq,m_n}(t) = \left[\exp\left(-\tau_{pq,m_n}(t) \frac{r_\tau - 1}{r_\tau \sigma_\tau}\right) 10^{-\frac{Y_n}{10}} \right] \quad (27)$$

where Y_n is the per cluster shadowing term following a Gaussian distribution. The final ray powers are obtained by normalizing $P'_{pq,m_n}(t)$ as

$$P_{pq,m_n}(t) = P'_{pq,m_n}(t) / \sum_{n=1}^{N(t)} \sum_{m_n=1}^{M_n} P'_{pq,m_n}(t). \quad (28)$$

III. STATISTICAL PROPERTIES

A. Time-Variant Delay PSD

The delay PSD $\Lambda_{pq}(t, \tau)$ intuitively reveal the power distribution the in time delay domain and is defined as

$$\Lambda_{pq}^\tau(t, \tau) = \sum_{n=1}^{N(t)} \sum_{m_n=1}^{M_n} P_{pq,m_n}(t) \delta(\tau - \tau_{m_n}(t)). \quad (29)$$

The temporal variation of delay PSD is caused by evolutions of clusters with respect to time. The variation trend of delay PSD will depend on the geometrical relationship updates of the underground scattering environment.

B. Local STF-CF

To study the correlation characteristics, the local STF-CF between $h_{pq}(t, f)$ and $h_{\tilde{p}\tilde{q}}(t - \Delta t, f - \Delta f)$ is defined as

$$R_{pq,\tilde{p}\tilde{q}}(t, f; \Delta d, \Delta t, \Delta f) = \mathbb{E}\{h_{pq}(t, f) h_{\tilde{p}\tilde{q}}^*(t - \Delta t, f - \Delta f)\} \quad (30)$$

where f and Δf denote the baseband frequency and frequency difference, respectively. The spatial difference $\Delta d = \{\Delta d_T, \Delta d_R\}$ contains antenna element spacings at Tx and Rx, that is, $\Delta d_T = \delta_{\tilde{p}} - \delta_p$ and $\Delta d_R = \delta_{\tilde{q}} - \delta_q$. Substituting (3) into (30), the local STF-CF can be obtained by sum of the correlation of the LoS component and the correlation of the NLoS components as

$$\begin{aligned} R_{pq,\tilde{p}\tilde{q}}(\Delta d, \Delta t, \Delta f; t, f) &= \frac{K_R}{K_R + 1} R_{pq,\tilde{p}\tilde{q}}^{\text{LoS}}(\Delta d, \Delta t, \Delta f; t, f) \\ &+ \frac{1}{K_R + 1} \sum_{n=1}^{N(t)} R_{pq,\tilde{p}\tilde{q},n}^{\text{NLoS}}(\Delta d, \Delta t, \Delta f; t, f). \end{aligned} \quad (31)$$

The STF-CF of LoS component is calculated as

$$\begin{aligned} R_{pq,\tilde{p}\tilde{q}}^{\text{LoS}}(\Delta d, \Delta t, \Delta f; t, f) &= [P_{pq}^{\text{LoS}}(t) P_{\tilde{p}\tilde{q}}^{\text{LoS}}(t - \Delta t)]^{\frac{1}{2}} \\ &\cdot e^{j \frac{2\pi(f_c - f)}{\lambda_{fc}} [D_{pq}^{\text{LoS}}(t) - D_{\tilde{p}\tilde{q}}^{\text{LoS}}(t - \Delta t)]} \cdot e^{j \frac{2\pi \Delta f}{\lambda_{fc}} [D_{\tilde{p}\tilde{q}}^{\text{LoS}}(t - \Delta t)]}. \end{aligned} \quad (32)$$

As for the local STF-CF of NLoS components, it can be calculated as

$$R_{pq,\bar{p}\bar{q},n}^{\text{NLoS}}(\Delta d, \Delta t, \Delta f; t, f) = P_s(t, \Delta t) \cdot \mathbb{E} \left\{ \sum_{m_n=1}^{M_n} a_{m_n} \cdot e^{j \frac{2\pi(f_c-f)}{\lambda_{jc}}} [D_{pq,m_n}(t) - D_{\bar{p}\bar{q},m_n}(t-\Delta t)] \cdot e^{j \frac{2\pi\Delta f}{\lambda_{jc}}} [D_{\bar{p}\bar{q},m_n}(t-\Delta t)] \right\} \quad (33)$$

where a_{m_n} is the amplitude that can be expressed by $a_{m_n} = [P_{pq,m_n}(t)P_{\bar{p}\bar{q},m_n}(t-\Delta t)]^{\frac{1}{2}}$, and $P_s(t, \Delta t)$ is the probability of the cluster surviving in period from $t - \Delta t$ to t .

C. Doppler PSD

The movement of the Tx and Rx will bring shift in the carrier frequency, which is called Doppler frequency shift. Doppler PSD reflects the distribution of signal power at different Doppler frequencies, which can be obtained by the Fourier transform of the temporal autocorrelation function (ACF)

$$S_n(\nu, t) = \int_{-\infty}^{\infty} r_n(t, \Delta t) e^{-j2\pi\nu\Delta t} d\Delta t \quad (34)$$

where ν is the Doppler frequency in Hz and $r_n(t, \Delta t)$ is the temporal ACF, which can be obtained by zeroing the Tx/Rx antenna spacing in the local STF-CF.

D. Stationary Interval

The nonstationary property can be characterized by the stationary interval, which is defined as the maximum duration within which the channel can be seen as stationary. For mobile communication systems, the channel estimation frequency greatly depends on the value of the stationary interval.

Here, we introduce the method of local region of stationarity (LRS) to obtain the stationary interval [44]. First, the average power delay profile (PDP) is obtained by taking average of N_{PDP} PDPs as

$$\bar{P}_h(t_k, \tau) = \frac{1}{N_{\text{PDP}}} \sum_k^{k+N_{\text{PDP}}-1} \Lambda_{pq}^\tau(t_k, \tau). \quad (35)$$

The average time is chosen as $N_{\text{PDP}} = 10$. The correlation coefficient between the average PDPs is defined as

$$c(t_k, \Delta t) = \frac{\int \bar{P}_h(t_k, \tau) \cdot \bar{P}_h(t_k + \Delta t, \tau) d\tau}{\max \left\{ \int \bar{P}_h(t_k, \tau)^2 d\tau, \int \bar{P}_h(t_k + \Delta t, \tau)^2 d\tau \right\}}. \quad (36)$$

Next the stationary interval is obtained as the largest time duration within which the correlation coefficient beyond the certain threshold c_{thresh} , that is,

$$T_s(t) = \max \{ \Delta t | c(t, \Delta t) \geq c_{\text{thresh}} \}. \quad (37)$$

According to most current investigations, the correlation coefficient threshold is empirically set to 90% and certainly this value can be adjusted according to specific requirements [5].

E. Angular Power Spectrum

The angular power spectrum reflects the distribution of channel power in angular domain. It can be acquired by power and angular parameters, and can be expressed as

$$\Lambda_{pq}^R(t, \phi_A^R, \phi_E^R) = \sum_{n=1}^{N(t)} \sum_{m_n=1}^{M_n} P_{pq,m_n}(t) \times \delta(\phi_A^R - \phi_{A,m_n}^R) \times \delta(\phi_E^R - \phi_{E,m_n}^R) \quad (38)$$

where ϕ_A^R and ϕ_E^R are AAoA and EAoA, respectively. Similarly, at the Tx side, the angular power spectrum can be obtained by the same method.

F. LCR and AFD

The LCR and AFD describe how quickly the channel changes over time and are essential parameters in the design and evaluation of communication systems. The LCR is defined as the number of occurrences per unit time that the amplitude of the channel crosses a given threshold bottom-up (or top-down). The LCR of a channel model can be calculated by the following equation [45]:

$$N(r, t) = \frac{2r\sqrt{K_R+1}}{\pi^{3/2}} \sqrt{\frac{b_2(t)}{b_0} - \frac{b_1^2(t)}{b_0^2}} e^{-K_R - (K_R+1)r^2} \times \int_0^{\pi/2} \cosh\left(2\sqrt{K_R(K_R+1)}r \cos \omega\right) \times \left[e^{-(\chi(t) \sin \omega)^2} + \sqrt{\pi} \chi(t) \sin \omega \operatorname{erf}(\chi(t) \sin \omega) \right] d\omega \quad (39)$$

where $\cosh(\cdot)$ refers to the hyperbolic cosine function and $\operatorname{erf}(\cdot)$ denotes the error function. Parameters $\chi(t)$ and $b_l(t)$ ($l = 0, 1, 2$) are written as

$$\chi(t) = \sqrt{\frac{K_R \cdot b_1(t)^2}{b_0 \cdot b_2(t) - b_1(t)^2}}. \quad (40)$$

According to the definition of temporal ACF, the $b_l(t)$ ($l = 0, 1, 2$) can be obtained as

$$b_l(t) = \frac{(2\pi)^l}{(K_R+1)\lambda^l} \cdot \sum_{n=1}^{N(t)} \sum_{m_n=1}^{M_n} P_{pq,m_n}(t) \left(\vec{v}_T \cdot \vec{r}_{m_n}^T / |\vec{r}_{m_n}^T| + \vec{v}_R \cdot \vec{r}_{m_n}^R / |\vec{r}_{m_n}^R| - \vec{v}_A \cdot \vec{r}_{m_n}^T / |\vec{r}_{m_n}^T| - \vec{v}_Z \cdot \vec{r}_{m_n}^R / |\vec{r}_{m_n}^R| \right)^l. \quad (41)$$

The AFD is defined as the average time duration of the envelope amplitude under the certain threshold, which can be calculated according to LCR, that is,

$$L(r, t) = \frac{1 - Q\left(\sqrt{2K_R}, \sqrt{2(K_R+1)}r^2\right)}{N(r, t)} \quad (42)$$

where $Q(\cdot)$ is the Marcum-Q function. Note that the calculation of the LCR and AFD in this article is based on the narrowband assumption, that is, the time delay difference between different clusters is not taken into account.

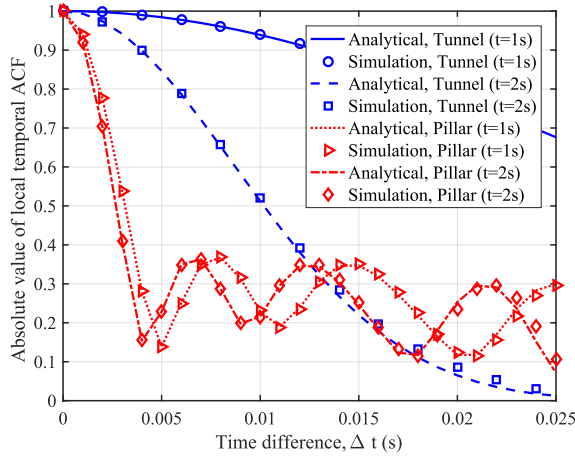


Fig. 5. Temporal ACFs at different scenarios and time instants ($v_T(t_0) = 10$ m/s, $a_T = 3$ m/s², $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, $\beta_E^{T(R)} = 0$).

IV. RESULTS AND ANALYSIS

In this section, the simulation of statistical characteristics based on proposed channel model is provided. The channel simulation is realized on personal computer (Intel(R) Core(TM) i7-9700 CPU @3.0 GHz, 32.0 GB RAM) using MATLAB R2016. In the simulation, the observation time is [1s, 2s], the Tx and Rx are equipped with uniform linear arrays with the antenna spacing δ_T and δ_R . Therefore, the distance from A_1^T to A_q^T and from A_1^R to A_q^R can be expressed as $(p-1)\delta_T$ and $(q-1)\delta_R$, respectively. The default parameters are set as follows: $f_c = 2.5$ GHz, $\tilde{p}(\tilde{q}) = 2$, $p(q) = 1$, $\beta_A^{T(R)} = \pi/3$, and $\beta_E^{T(R)} = 0$. For the tunnel scenario, the generation and recombination rates are set to $\lambda_G = 20$, $\lambda_R = 1$ at near-field, and $\lambda_G = 5$ and $\lambda_R = 1$ at far-field. For the pillar scenario, the scatterer density is set to 0.002/m³. The observable regions at Tx and Rx sides are spheres taking Tx and Rx as centers with 20 m radius. In addition, the simulation in this section are based on the horizontal propagation assumptions and the use of omnidirectional antennas at the Tx and Rx.

Fig. 5 shows the absolute value of the temporal ACF at different time instants for different scenarios. In the simulation, Rx is accelerated in a straight line with an initial velocity of 10 m/s and an acceleration of 3 m/s². It is found that the absolute value of the temporal ACF is larger in the tunnel scenario than in the pillar scenario. It may be because the parameters of MPCs are similar in the tunnel scenario, while the parameters of MPCs are different in the pillar scenario. In addition, since the speed of Rx is set to the acceleration motion, the channel change rate gradually becomes larger so the temporal ACF gradually decreases. Finally, we compare the theoretical results and simulation results of different scenarios at different times, and the two fit well, reflecting the consistency of channel characteristic derivation and simulation.

Fig. 6 presents the absolute values of the spatial cross-correlation function (CCF) for different scenarios and antenna orientations. Since the MPCs come from similar directions in the tunnel scenario, the absolute value of the spatial CCF is larger in the tunnel scenario. This means that larger spatial complexing gain can be achieved in the pillar scenario. In addition, we can find that antenna orientation angle variation has a more significant effect on the spatial correlation in

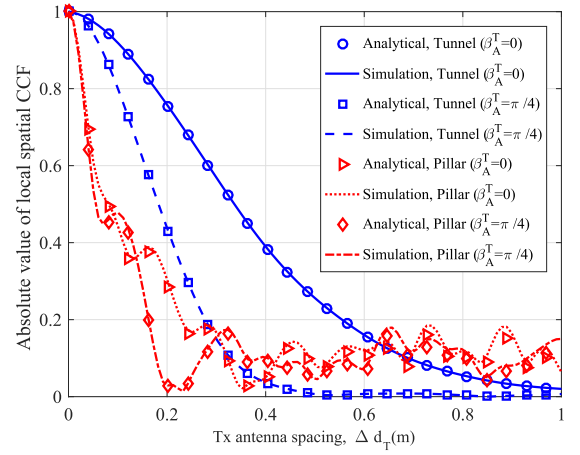


Fig. 6. Spatial CCFs at different scenarios and antenna array broadsides ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^R = \pi/3$, and $\beta_E^{T(R)} = 0$).

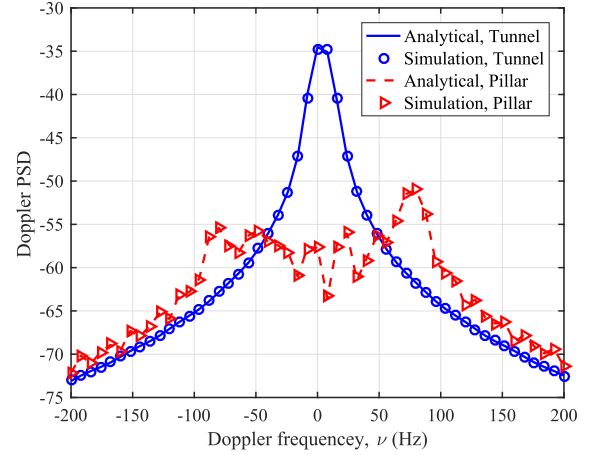


Fig. 7. Doppler PSD in different scenarios ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$ and $\beta_E^{T(R)} = 0$).

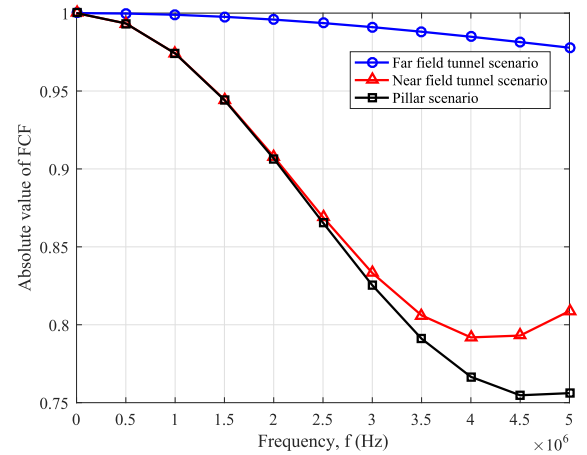


Fig. 8. FCFs in different scenarios ($f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, $\beta_E^{T(R)} = 0$; pillar scenario and tunnel scenario near field: $\sigma_\tau = 10^{-7.5}$; tunnel scenario far-field: $\sigma_\tau = 10^{-8.5}$).

the tunnel scenario, while antenna orientation angle variation has a less significant effect on the spatial correlation in the pillar scenario.

Fig. 7 gives the Doppler PSD for different structure scenarios. It can be found that the Doppler PSD is more concentrated in the tunnel scenario, with larger power peaks

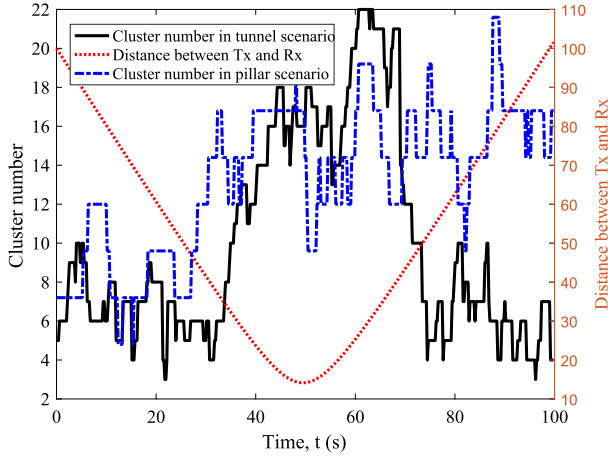


Fig. 9. Cluster number in different scenarios ($v_T(t_0) = 2$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, $\beta_E^{T(R)} = 0$).

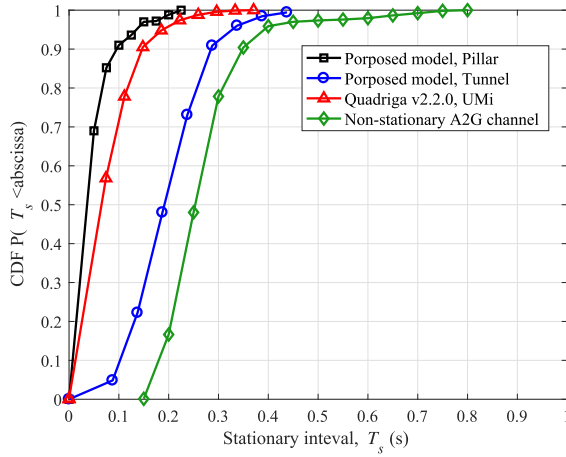


Fig. 10. Stationary intervals of different scenarios and different channel models ($v_T(t_0) = 4$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, $\beta_E^{T(R)} = 0$).

appearing, while the Doppler PSD is more dispersed in the pillar scenario, close to the U-shaped power spectrum in the isotropic channel scenario to a certain extent.

Fig. 8 presents the frequency correlation functions (FCFs) for pillar scenario and near/far fields in the tunnel scenario. The FCF represents the variation of the channel in the frequency domain. It can be observed that FCF descends slower in the far-field tunnel scenario, while FCFs in the pillar scenario and the near-field tunnel scenario have the similar variation trends. Usually coherent bandwidth is chosen as the bandwidth meeting the condition that FCF exceeds 90% threshold. Under the given parameter setting, the coherent bandwidths of the near-field tunnel channel and the pillar channel are about 2 MHz and that of the far-field tunnel channel is about 10 MHz, indicating more flat fading in the far-field tunnel channel.

Fig. 9 shows the path number in different structure scenarios. As the distance between Tx and Rx increases, due to the switching of channel parameters from near-field to far-field, the number of clusters in the tunnel scenario gradually decreases from 22 to 5, while for the pillar scenario, the number of clusters presents random fluctuation and distance between Tx and Rx has no significant effect on the number of clusters.

Fig. 10 gives the simulation results of stationary interval of different scenarios. It can be observed that the stationary

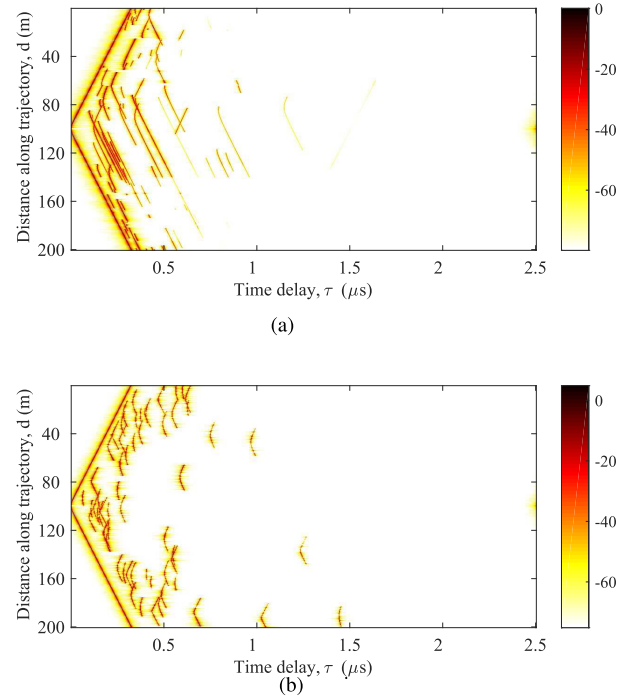


Fig. 11. Time-variant time-delay PSD of the proposed underground channel model ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, and $\beta_E^{T(R)} = 0$). (a) Time-delay PSD in the tunnel scenario. (b) Time-delay PSD in the pillar scenario.

intervals of the pillar scenario are smaller than those of the tunnel scenario, which illustrates that a higher channel estimation frequency should be used in the pillar scenario. Besides, we also provide the simulation results of existing channel models for comparison. Since that simple stochastic channel models such as traditional Rayleigh and Ricean models are based on the wide-sense-stationary assumption, they cannot characterize the time-variant environment and nonstationary propagation property. To quantify the nonstationary property in underground scenarios, we choose two nonstationary channel models, that is, quasi-deterministic radio channel generator (QuaDRiGa) [43] and nonstationary air-to-ground (A2G) channel model [31] for reference. The scenario of QuaDRiGa is set as overground urban micro (UMi) cell and scenario of nonstationary A2G channel model is set as an urban area with UAV height $h_U = 100$ m. With the same system configuration (carrier frequency, velocity, etc.) and stationary interval calculation method, it can be noticed that the stationary interval in the pillar scenario is shorter than stationary intervals of UMi and A2G scenarios. The reason is the dense distribution of scatterers in the pillar scenario. The distribution of the stationary interval in the tunnel scenario is between those of UMi and A2G scenarios because the A2G channel has more dominant LoS components. The analysis of nonstationary property can provide some references and guidance for the underground communication system design from the perspective of the propagation channel. For instance, the smaller stationary interval in the pillar scenario means that a higher channel estimation frequency should be considered in the system design.

Fig. 11 illustrates the delay PSD of different structure scenarios. The Rx trajectory is set to a linear track that comes close to Tx first and then moves away. In both the tunnel and pillar scenarios, it can be observed that the power of MPC

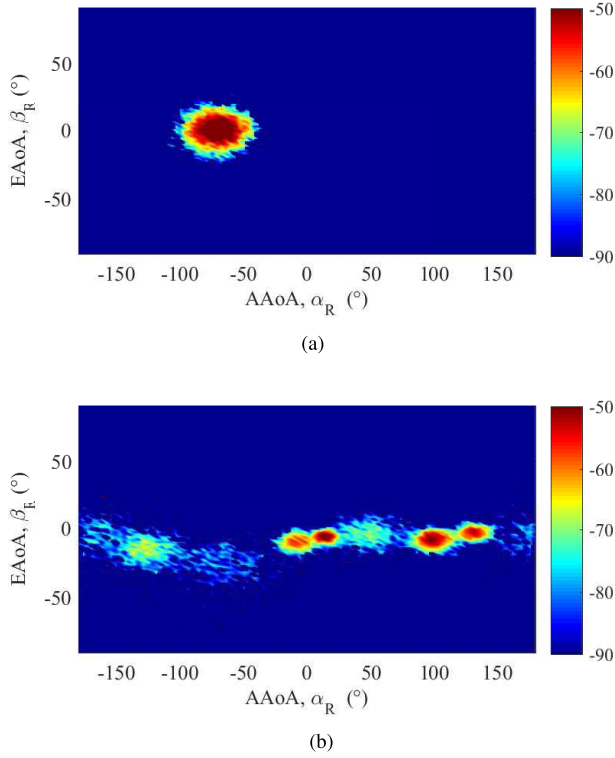


Fig. 12. Angular PSD of the proposed underground channel model ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, and $\beta_E^{T(R)} = 0$). (a) Angular PSD in the tunnel scenario. (b) Angular PSD in the pillar scenario.

gradually decreases and the delay of MPC gradually increases with the increasing distance between Tx and Rx. In the moving process, birth death of MPCs and drifting of powers and delays can be found both in the pillar and tunnel scenarios.

Fig. 12 shows angular PSDs at Rx for different structure scenarios. Without the loss of generality, we assume that both Tx and Rx are equipped with omnidirectional antennas. It can be observed that the multipath mostly coming from one direction with a higher concentration in the tunnel scenario. In the pillar scenario, the multipath comes from scattered clusters in different directions, with a large spread in the azimuth angle and a smaller spread in the elevation angle due to the top and bottom limitations.

Figs. 13 and 14 provide the simulation of LCR and AFD for different structure scenarios. Under the same Tx/Rx motion states, the tunnel structure scenario has the lower LCR and larger AFD, representing the slower channel time-varying. The pillar scenario has a higher LCR and smaller AFD, representing the faster channel time-varying.

V. CHANNEL MODEL VALIDATION

A. Channel Measurement Setup

To validate the proposed model, underground channel measurement is conducted based on our Keysight time-domain channel sounder in the underground garage of Shandong University, Qingdao Campus. The garage is about 120 m long, 40 m width, and 4 m height. The 3-D map of this garage and photograph taken during measurement are provided in Fig. 15. As shown in Fig. 16, the channel sounder Tx side consists of an M8190A arbitrary waveform generator (AWG) with a sampling rate of 12 GSa/s, an E8267D vector signal generator (VSG) with a frequency range of 100 kHz to 44 GHz,

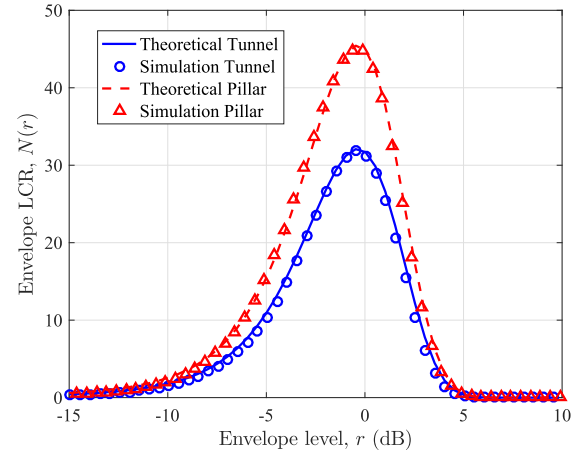


Fig. 13. LCR in different scenarios ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, and $\beta_E^{T(R)} = 0$).

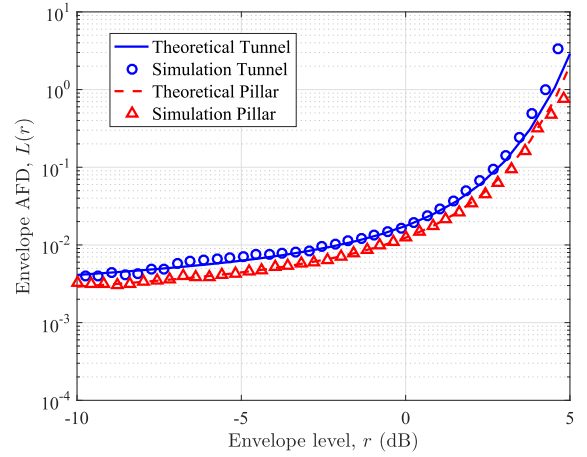


Fig. 14. AFD in different scenarios ($v_T(t_0) = 10$ m/s, $f_c = 2.5$ GHz, $\beta_A^{T(R)} = \pi/3$, and $\beta_E^{T(R)} = 0$).

a high-precision HJ5418 GPS Rubidium clock, and a power amplifier (PA). The Rx side consists of an M9362A PXIe down converter, an M9352A PXI hybrid amplifier/attenuator, an M9300A PXIe frequency reference, an M9703B AXIe 12-bit digitizer, an E8257D analog signal generator, a GPS Rubidium clock, and a low noise amplifier (LNA). More detailed information of this sounder system is available in [46].

Due to the limitations of the available number of Tx/Rx antennas and PA/LNA, the channel measurement is conducted in the single-input single-output (SISO) mode. Omnidirectional discone antennas working in the range of 0.1–6 GHz with 2 dBi gain are utilized at both Tx and Rx sides. To enhance the effective measurement distance, a PA with 28 dB gain and an LNA with 35 dB gain are equipped at Tx and Rx sides, respectively. The measurements are conducted at 2.5 and 3.5 GHz bands with 625 MHz bandwidth. To enlarge the measurement system dynamic range, the pseudo-noise (PN) sequence with a length of $2^{12} = 4096$ is utilized as the baseband measurement waveform, and a processing gain of $G_{wa} = 10\log_{10}2^{12} = 36$ dB is realized. Considering the standard thermal noise power density as -174 dBm/Hz, the receiving noise power is $P_n = -174$ dBm/Hz + 88 dBHz + 35 dB = -51 dBm. Taking

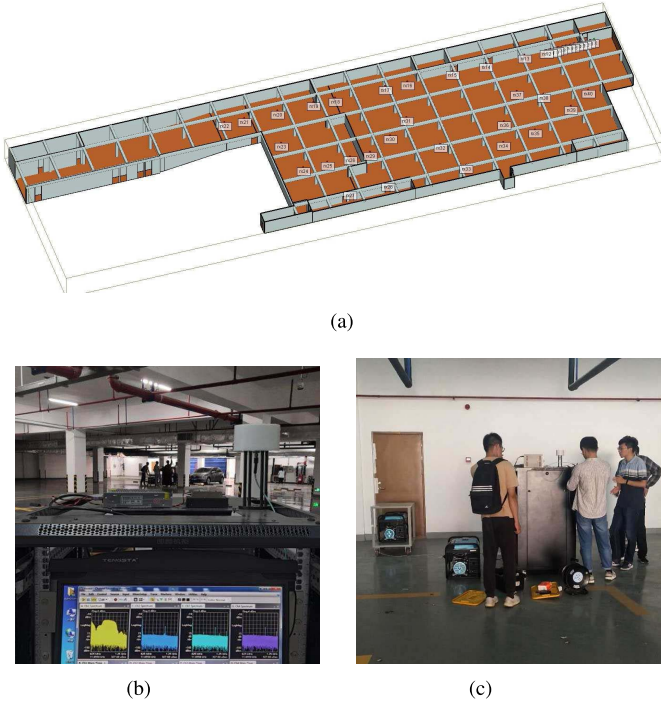


Fig. 15. Underground channel measurement scenario. (a) 3-D map of measurement garage. (b) Measurement process (Rx side). (c) Measurement process (Tx side).

$P_m = 5$ dB as margin, the dynamic range can be obtained as

$$D_r = P_t + G_{PA} + G_t + G_r + G_{LNA} + G_{wa} - P_n - P_m - L_{sys} = 146 \text{ dB} \quad (43)$$

where G_t and G_r are the gains of Tx and Rx antenna, respectively, G_{PA} is the gain of the PA, $P_t = 0$ dBm is the power of the transmitting signal, G_{LNA} is the gain of LNA, and $L_{sys} = 10$ dB is the attenuation caused by the measurement system (including attenuations of cable, adapter, etc.). This value of dynamic range means that measurement system can identify the MPC with maximum attenuation as 146 dB.

Besides, 404 and 500 zero points are added at the start and end of the waveform, respectively, to leave the time for amplifier response of power ramp up/down. To mitigate the inter symbol interference (ISI), the transmitted waveform is interpolated with two times and filtered by a root raised cosine (RRC) pulse shaping filter with a roll-off factor of 0.35. The received signal is also filtered by the same matched filter and down-sampled with two times.

In the measurement, the Rx is fixed at the entrance of garage, and Tx is slowly moving in the garage. At both 2.5 and 3.5 GHz bands, we measure 40 points in the garage. The scenario layout and the coordinates of these points are marked in Fig. 15(a).

B. Measurement Data Processing

To eliminate the frequency response brought by the sounder, we first use back-to-back calibration signal to calibrate the measurement system [46], and obtain the attenuation and time delay of the signal caused by the measurement system. Then the relative CIRs at each measurement points can be calculated by

$$h(\tau) = \text{IFFT}(H(f)) = \text{IFFT}(Y_{rx}(f)/X_{tx}(f)) \quad (44)$$

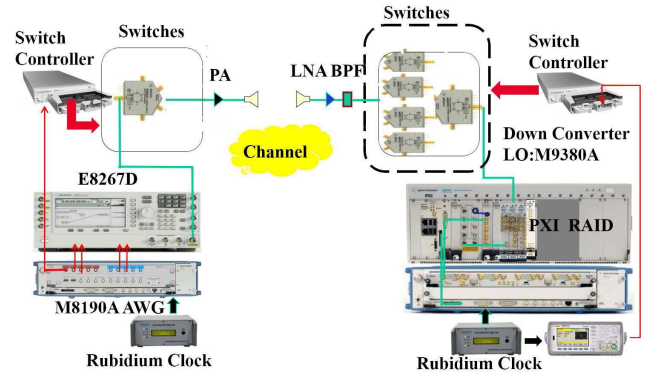


Fig. 16. Keysight time-domain channel sounder.

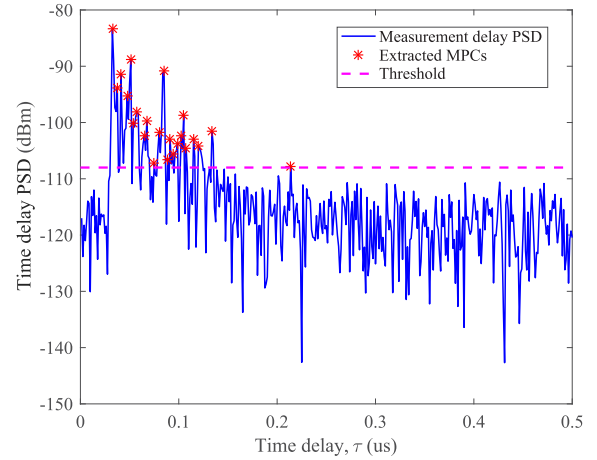


Fig. 17. Measurement continues delay PSD and extracted MPCs at point 38.

where $X_{tx}(f)$ and $Y_{rx}(f)$ are frequency-domain responses of transmitting and receiving signals, respectively.

The MPCs can be extracted by the peak search algorithm in continuous delay PSD, that is, $|h(\tau)|^2$. The complex amplitude, power, and time delay of the l th MPC are denoted by h_l , P_l , and τ_l , respectively. The peak searching power threshold is chosen as maximum value between maximum power minus 20 dB and average noise floor plus 5 dB [46]. The MPCs extracting result at point 38 is presented in Fig. 17. The received power P_r is calculated by summing all powers of MPCs. To characterize the large-scale fading, the path loss is given by

$$PL(\text{dB}) = -P_r + G_t + G_r + G_{PA} + P_t + G_{LNA} - L_{sys}. \quad (45)$$

To keep consistency between channel measurement and model simulation in small-scale fading characteristic analysis, the measurement MPC powers at each measurement point are normalized same as (28) and normalized received signal envelope can be obtained by

$$a = \sum_{l=1}^L h_l e^{2\pi f \tau_l} \cdot \left(\sum_{l=1}^L P_l \right)^{-1/2}. \quad (46)$$

To characterize the time delay properties, the root mean square (rms) delay spread can be expressed by

$$\sigma_\tau = \sqrt{\frac{\sum_{l=1}^L P_l \tau_l^2}{\sum_{l=1}^L P_l} - \left(\frac{\sum_{l=1}^L P_l \tau_l}{\sum_{l=1}^L P_l} \right)^2}. \quad (47)$$

TABLE IV
FREQUENCY-SPECIFIC FITTING PARAMETERS

Parameters	A	n	K_R (dB)	σ_τ (dB)	r_τ	σ_n
2.5 GHz	-39.32	1.96	12.0	-7.31	2	2.5
3.5 GHz	-39.27	2.19	10.2	-7.53	2	2.5

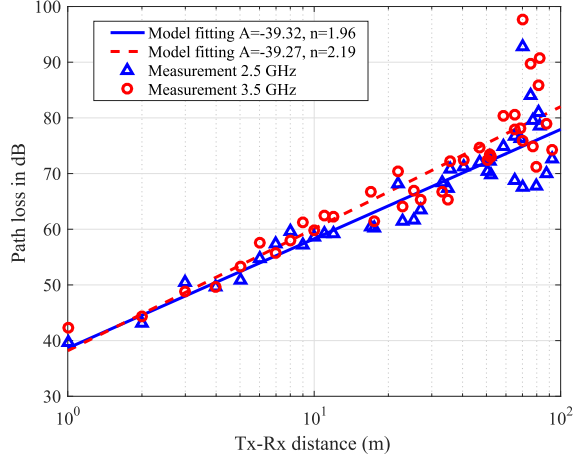


Fig. 18. Measurement path loss and fitting results at 2.5 and 3.5 GHz.

C. Comparison With Measurement Data

To ensure the accuracy and usefulness of the proposed channel model, we use the channel measurement data to validate the proposed channel model. The simulation parameter set is estimated based on the minimum mean square error (MMSE) criterion, that is, $\varepsilon = |\hat{F} - F(\mathcal{P})|^2$, in which $\hat{F}$ is the measurement statistical property such as CDF of the amplitude, F is the derived statistical property, and $\mathcal{P}$ is the estimated parameter set. Note that only a small number of parameters have significant influence on the targeted statistical property, so estimated parameter set $\mathcal{P}$ only includes a part of simulation parameters.

The path loss measurement results and model fitting results are shown in Fig. 18. Since the garage size limitation, the measurement distance is in the range of 1–100 m. It can be observed that path losses increase linearly with log distance between Tx and Rx at 2.5/3.5 GHz bands. Due to the limitation of measurement distance, the break point is not found in our measurement result. Substituting cross section width $w = 40$ m and height $h = 4$ m in (2), the break point distances can be calculated as 16 km at 3.5 GHz and 13 km at 2.5 GHz, which are greater than the maximum measurement distance. Therefore, the single slope path loss model is used in fitting. The 3.5 GHz band has the larger path loss exponent compared to 2.5 GHz band. It is worth mentioning that path loss exponent at 2.5 GHz ($n = 1.96$) is a little bit smaller than that of free space path loss ($n = 2$). Though a lot of obstacles exist in the pillar scenario, the path loss exponent in the measurement pillar scenario is still close to the free space path loss exponent. The reason behind may be the ceiling and floor forming a nonobvious waveguide structure.

For the small-scale fading, the measurement results of normalized signal amplitudes are provided in Fig. 19. It can be found that the CDFs of amplitudes at 2.5 and 3.5 GHz are similar, and the amplitudes at 2.5 GHz show slightly more dispersion. The fitting parameters including Ricean K factor

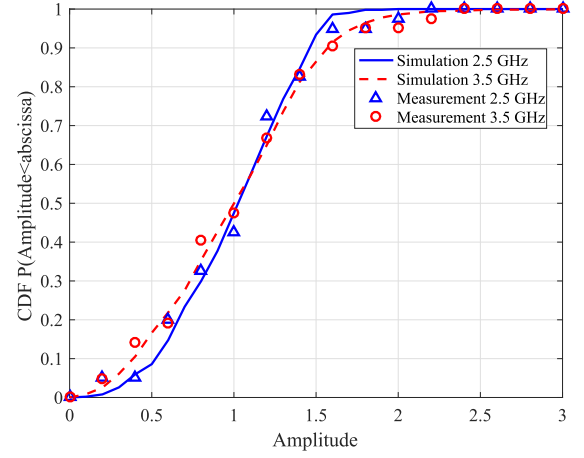


Fig. 19. Normalized measurement amplitudes and fitting results at 2.5 and 3.5 GHz.

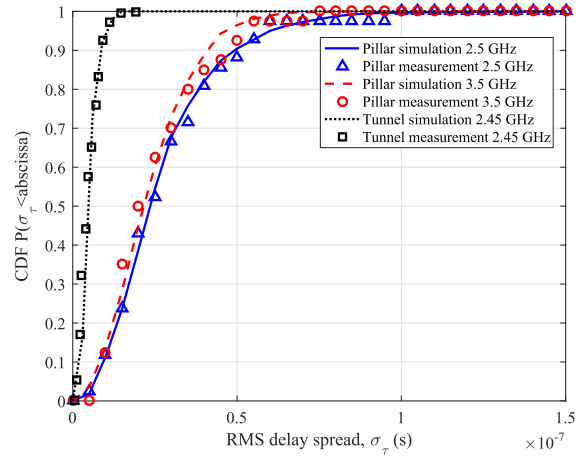


Fig. 20. Measurement rms delay spread and fitting results at 2.5 (2.45 GHz in the tunnel for reference [49]) and 3.5 GHz.

TABLE V
K-S TEST D VALUES FOR DIFFERENT STATISTICAL PROPERTIES

Statistical properties	Amplitude	RMS delay spread	95% significance upper quantile
2.5 GHz	0.04	0.06	0.21 [50]
3.5 GHz	0.07	0.08	

K_R and dispersion of cluster σ_n are provided in Table IV. For the time delay properties, the measurement rms delay spreads are shown in Fig. 20. The difference of delay spread between 2.5 and 3.5 GHz is less marked. Besides, the fitting parameters including the expectation of delay spread and per cluster spread are provided in Table IV. For comparison, the measurement rms delay spread at the tunnel scenario and the fitting results are also provided. Since there is no available tunnel measurement result at 2.5 or 3.5 GHz, the tunnel measurement result at adjacent frequency band 2.45 GHz is chosen for reference. The results are obtained in mine shaft by wideband-frequency domain measurement and detailed measurement set is available in [49]. From the comparison, it can be observed that at similar frequency bands, the rms delay spread at the tunnel scenario is much smaller than that of pillar scenario.

To further validate the accuracy of the proposed channel model, we implement the Kolmogorov–Smirnov (K–S) test to give an accuracy measure. The K–S test is widely used as a nonparametric test of equality for 1-D probability distributions. The K–S distance values (D values) between simulation results and measurement results for different statistical properties and frequencies are provided in Table V. Through the comparison, we can see that D values of the proposed model are far below the upper quantile of 95% significant level, indicating the accuracy and reliability of the proposed channel model.

VI. CONCLUSION

In this article, a general 3-D nonstationary model for underground vehicular channels has been proposed based on different underground space structure scenarios. Different cluster generation and evolution mechanisms for the pillar and tunnel scenarios have been introduced into the proposed model. Based on the proposed channel model, we have derived the statistical properties of different underground scenarios, including temporal ACF, spatial CCF, Doppler PSD, LCR, and AFD. The theoretical derivation results fit well with the simulation results, which verifies the correctness of both theoretical derivations and simulations. Based on the derived and simulated results, we have found that under the same Tx/Rx trajectory and antenna configuration, the channel is more stable and changes slower w.r.t. time in the tunnel scenario, while in the pillar scenario, the spatial correlation is usually smaller, that is, the larger spatial diversity gain can be achieved. In addition, underground channel measurements have been conducted to investigate channel characteristics at different frequency bands (2.5/3.5 GHz). Measurement and simulation results have been compared to verify the accuracy and practicality of our proposed model.

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